

Design, construction, and performance test of MICE superconducting solenoids

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Abstract—The purpose of the MICE spectrometer solenoid is to provide a uniform field for a scintillating fiber tracker, and thus, it is also called tracker solenoid. The uniform field is produced by a long center coil and two short end coils. Together, they produce 4T field with a uniformity of better than 1% over a detector region of 1000 mm long and 300 mm in diameter. Throughout most of the detector region, the field uniformity is better than 0.3%. In addition to the uniform field coils, we have match coil 1 and match coil 2. These two coils can be independently adjusted to match uniform field region to the focusing coil field. The overall coil package is 2544 mm. We shall present the tracker solenoid cold mass design, the cold mass support against 50 ton axial load, the cryogen free system equipped with cryocooler, recondenser, Hi-Tc lead, and the vacuum vessel. Finally, we shall present performance test data of the MICE tracker solenoids.

Index Terms— MICE, performance test, spectrometer, tracker solenoid.

I. MAGNET DESIGN

WE have designed a five-coil scintillating fiber tracker spectrometer solenoid which provide a 4T uniform field over a region 300 mm diameter by 1000 m long. The uniform field is provided by a long solenoid and two end coils. Two of the five coils, M_1 and M_2 are for beam focusing match and are independently adjustable. Fig. 1 shows the on-axis field profile and Fig. 2 shows the conductor used, the peak field and the load line. The coil design parameter is shown in Table I. The axial coil force, the maximum magnetic pressure, and the maximum coil stress are shown in Table I.

The five coils bobbin is machined from a single forged 6061T6 aluminum cylinder to contain the axial load. The radial load is further supported by aluminum band of 6 to 10 mm in thickness. The helium vessel shell is made of 12.7 mm 6061T6 aluminum. Table III summarize the inductance and stored energy calculation and Table IV summarized the result of 3D quench analyses. Fig. 3 shows magnet protection design and instrumentation.

Table I Coil Design and Actual Winding Data Summary

	M1	M2	E1	CENTRAL	E2
# TURN	115	114	84	788	84
# LAYER	42	28	59	20	52
TOTAL TURN	4830	3192	3584	15360	3066
Z1 (CM)	23416	464254	908879	1058851	2408879
Z2 (CM)	224584	663746	1019321	2371149	2519321
R1 (CM)	26.8	26.8	25.8	25.8	25.8
R2 (CM)	3044825	2886075	319059	280416	328263
DELTA Z (CM)	201188	199492	110842	1314298	110842
DELTA R (CM)	484825	308075	81859	22418	88263

Table II. Axial Coil Force, Maximum Axial Pressure and Coil Stress

41 ton	16 ton	105 ton	7 ton	169 ton
M1	M2	E1	C	E2
118 kg/cm ²	108 kg/cm ²	95 kg/cm ²	48 kg/cm ²	210 kg/cm ²
Maxim. Magnetic Pressure				

	coil	hoop stress (kg/cm ²)	compress stress (kg/cm ²)
M_1	match 1	538.8	-182.5
M_2	match 2	643.3	-124.7
E_1	end 1	834.7	-298.2
C	center	818.2	-39.6
E_2	end 2	882.7	208.9

Table III Inductance and Stored Energy

Coil	M1	M2	E1*	Center*	E2*	Total
Inductance(H)	17.47	9.59	15.39	51.58	15.91	109.94
Energy (MJ)	0.56	0.33	0.40	1.88	0.46	3.63
Operated Current	253.80	283.60	226.60	269.90	240.70	
*Total Inductance for Three Coil = 80.6700 H						

Table IV 3D Quench Analyses

Coil	M1	M2	E1	C (half)	E2
Quench time	2.4 sec	3.6 sec	4.4 sec	3 sec	4.2 sec
Maximum R	9.6 Ω	6.0 Ω	7.1 Ω	12.0 Ω	8.9 Ω
Maximum internal V	1143 V	454 V	857 V	1637 V	1094 V
Maximum temperature	135K	83K	131K	86K	155K

II. CRYOSTAT DESIGN

Design of cryostat and instrumentation is shown in Fig 4. The cryostat consists of 4.2K helium vessel, 60-80K thermal shield, and a 300K vacuum vessel. The total heat leak is shown in Table V and VI. The service tower is equipped with 3-1.5W pulsed-tube cryocoolers and 8 Hi-Tc leads to achieve zero cryogen boil off for the 5-ton cold mass magnet.

The helium vessel is designed to satisfy ASME pressure vessel code. The total liquid helium volume is about 180 liters. The helium vessel pressure rating is 45 psi. The rupture disc pressure is set at 30 psi. The relief pressure will be set at 10 psi.

The 60-80K shield is made of 6.35 mm thick 6061T6 aluminum. The shield is conduction cooled by the first stage of cryocooler. The vacuum vessel is made of 20 mm thick 304SS and is made to satisfy the ASME pressure vessel code to sustain a pressure rating of 1 atmosphere pressure. The helium vessel contains one precool tube (25 mm in diameter) and two vent

tubes of 38-mm diameter each. In addition, it has a 12-mm diameter gas recovery tube and one 6-mm diameter liquid refill tube for three helium recondensers.

The service tower is designed with three vacuum insulating sleeves to allow removal of cold head for maintenance without warming up the magnet. In addition to cool the thermal shield, the first stage of the cold head is employed to cool the hot end of high -T_c lead at 60K, as shown in Photo 1. The heat leak of 60-80K shield and of 4.2K is shown in Table V and Table VI.

III. COIL FABRICATION AND CRYOSTAT CONSTRUCTION

Photo 1 shows the coil winding fabrication and helium shell installation. The winding data is tabulated in Table I.

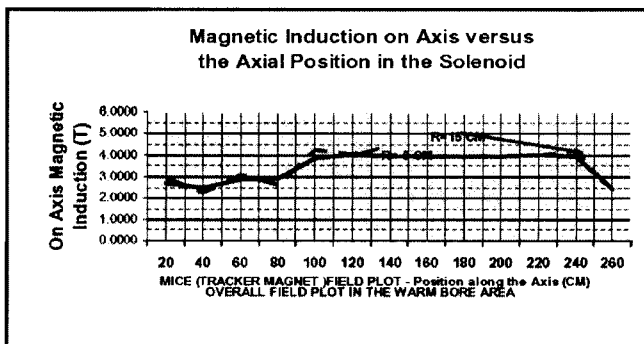
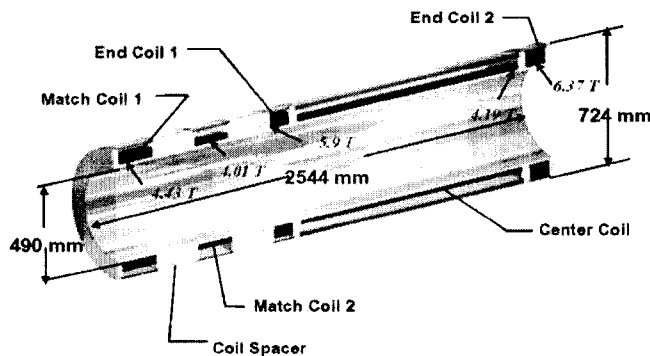
Photo 2 shows the cryostat assembly.

Photo 3 shows the service tower assembly with 3 cryocoolers, Hi-Tc lead, and thermal intercepts to remove I²R and many heat sinks to the first stage of cryocooler.

Table V Heat Leak to 80 K Shield

- (a) Heat leak through two neck tubes from 300 K through 80 K intercept = 1.888W
- (b) Radiation from 300 K to 80 K for total surface area(149468 cm²) = 10.745W
- (c) Heat leak through LN2 cold mass suspension = 0.58W
- (d) Heat Leak from 4.2 K cold mass suspension = 6.41W

Fig. 1 Tracker Solenoid Peak Field And On-Axial Field Profile



- (e) From Hi Tc lead = 91.5W
- Total heat leak = (a) through (e)=111 W

Table VI Heat Leak to 4.2 K if shield is 80 K

- (a) Two SS neck tubes conduction from 80 K to 4.2 K =56 mW
- (b) Three Cryocooler sleeve SS tube from 1st stage 60 K to 4.2 K =624 mW
- (c) Radiation from 80 K to 4.2 K =31.4 mW
- (d) Cold mass Suspension =308 mW
- (e) Hi Tc lead – =850 mW
- (f) Feedthru I²R Joint =1440 mW

Total Heat Leak to 4.2 K 3342mW = 3.342 W

IV. PERFORMANCE TEST OF MAGNET AND CRYOSTAT

To keep thermal stress at helium shell within 10 ksi, we control cool down to 1° K per hour. After we have filled liquid helium to cover 30% of coil, we performed magnet energization test. We have energized each of five coils. Then we energized all five coils together with 10-V 500 A power supply. It takes 5 training to reach 194 A. Before airship to UK. The magnet will be warm up and then ship to Fermi Laboratory to add end iron shield to test the effect of 50 ton attractive force to complete the last 50 A energization and to perform Final Field mapping.

Fig. 2 Conductor, Peak Field and Load Line Design

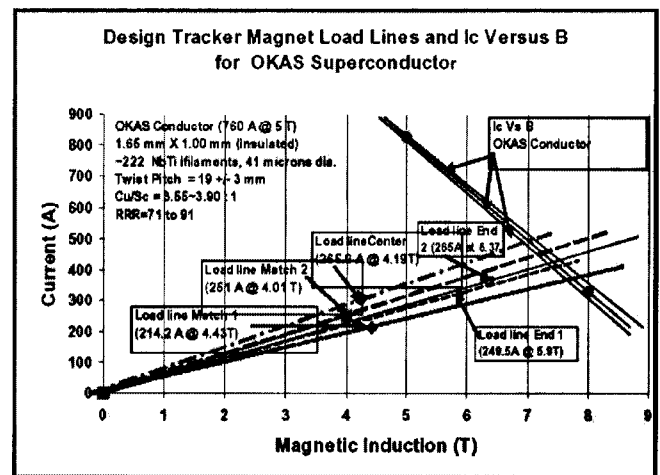


Fig.3 Magnet Protection

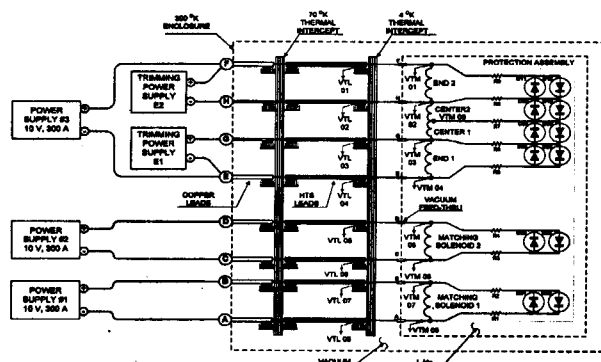


Fig.4

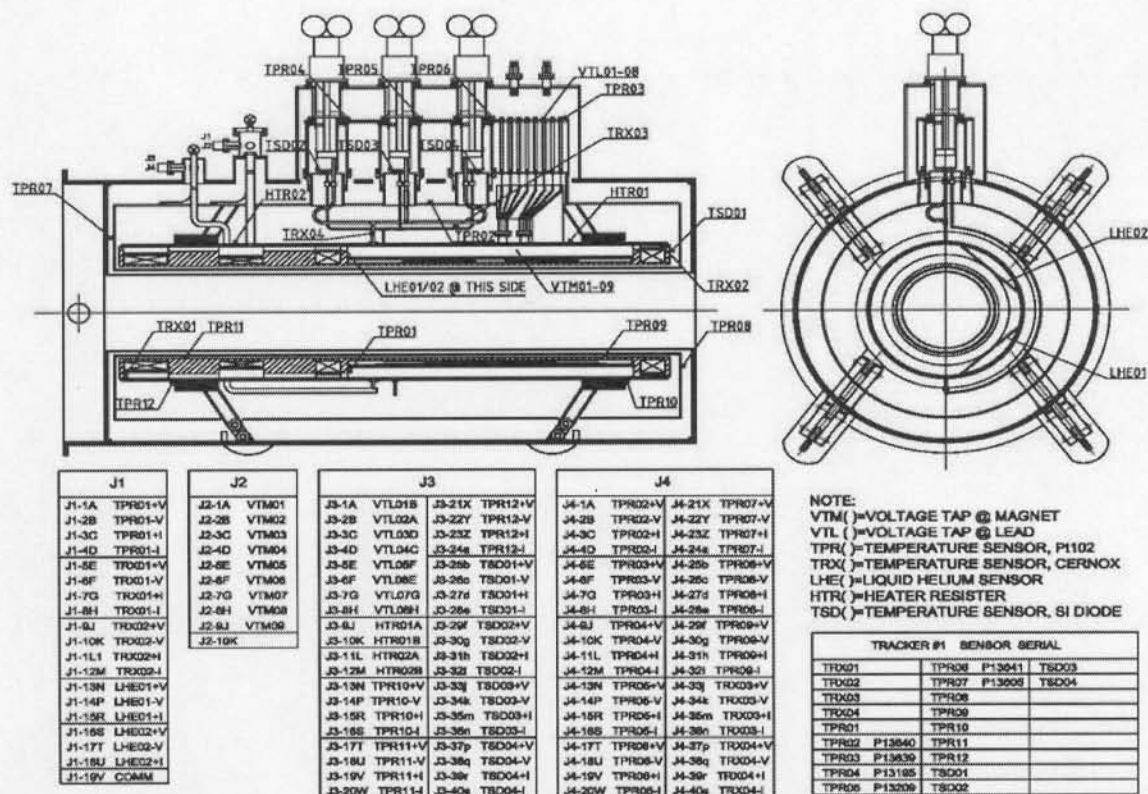
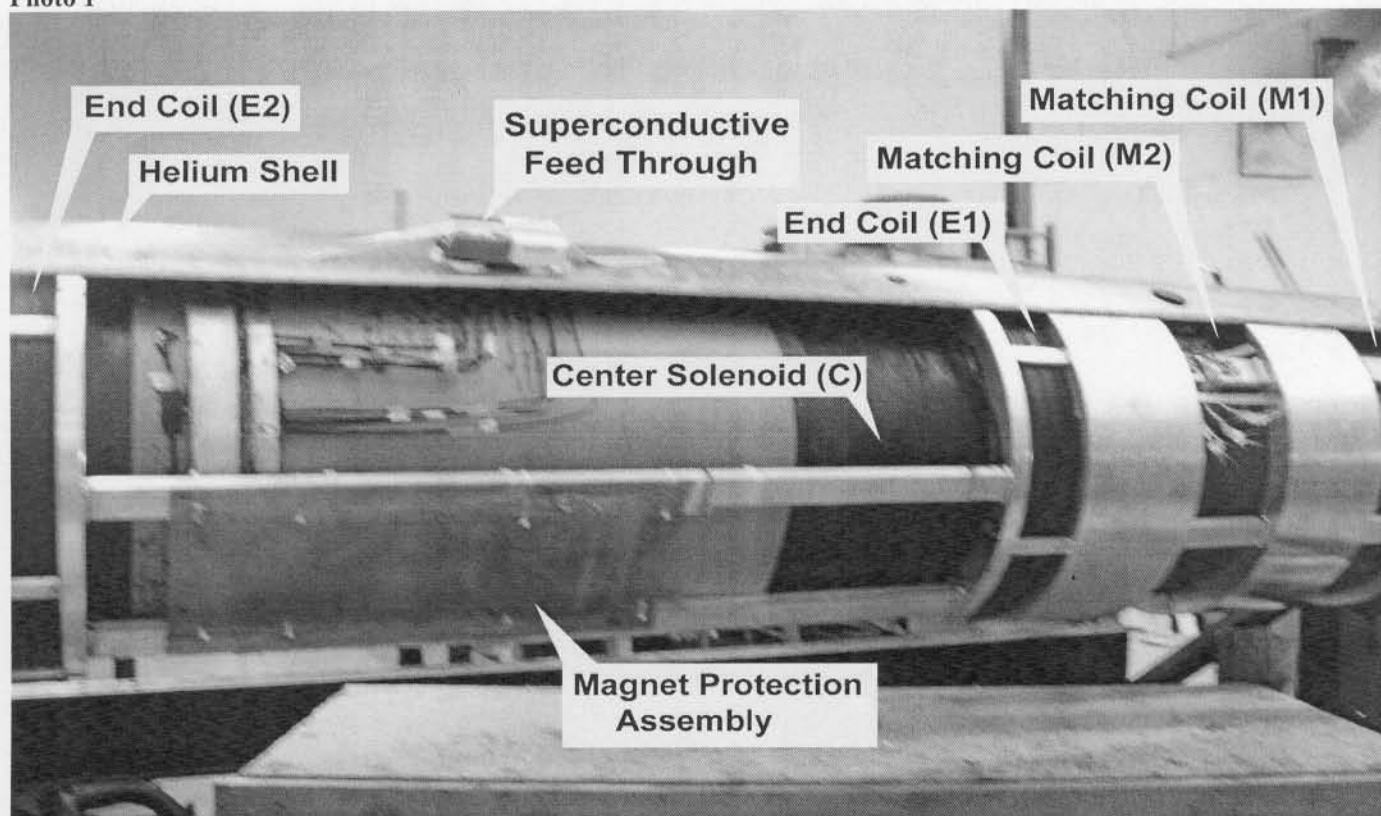
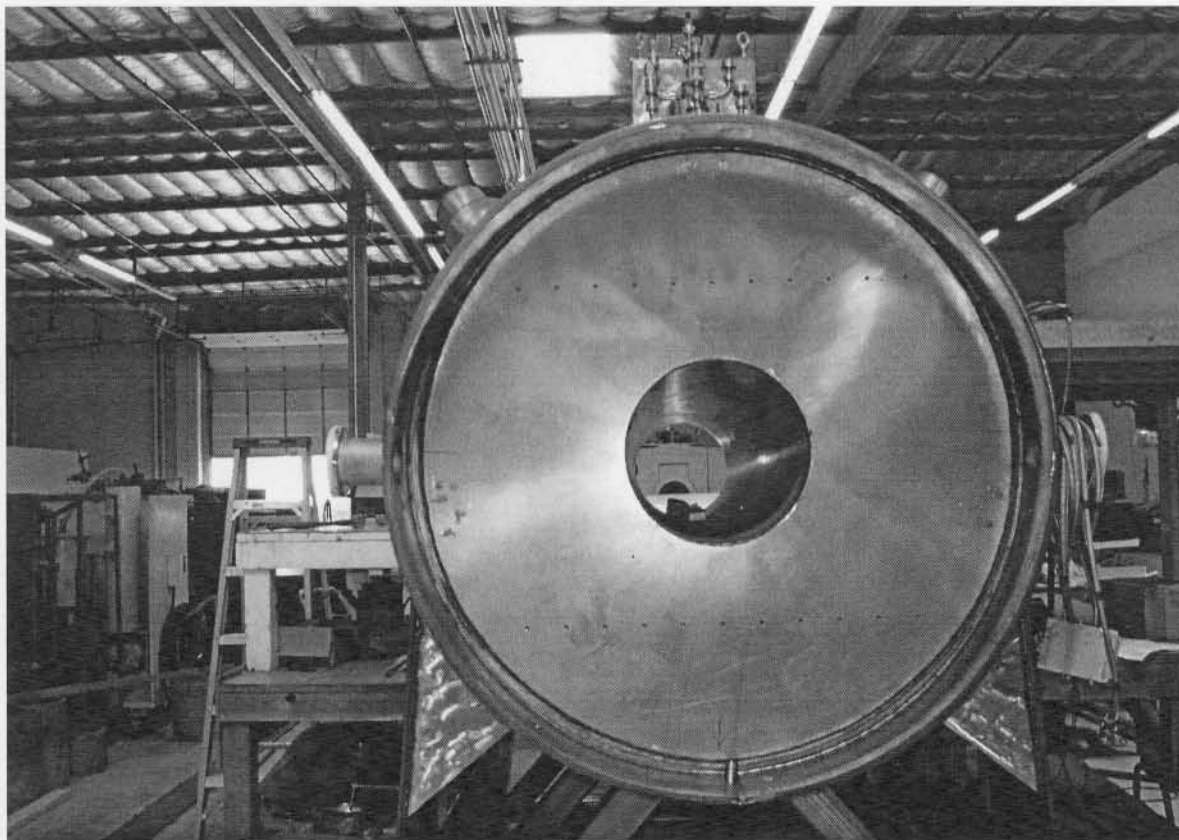


Photo 1



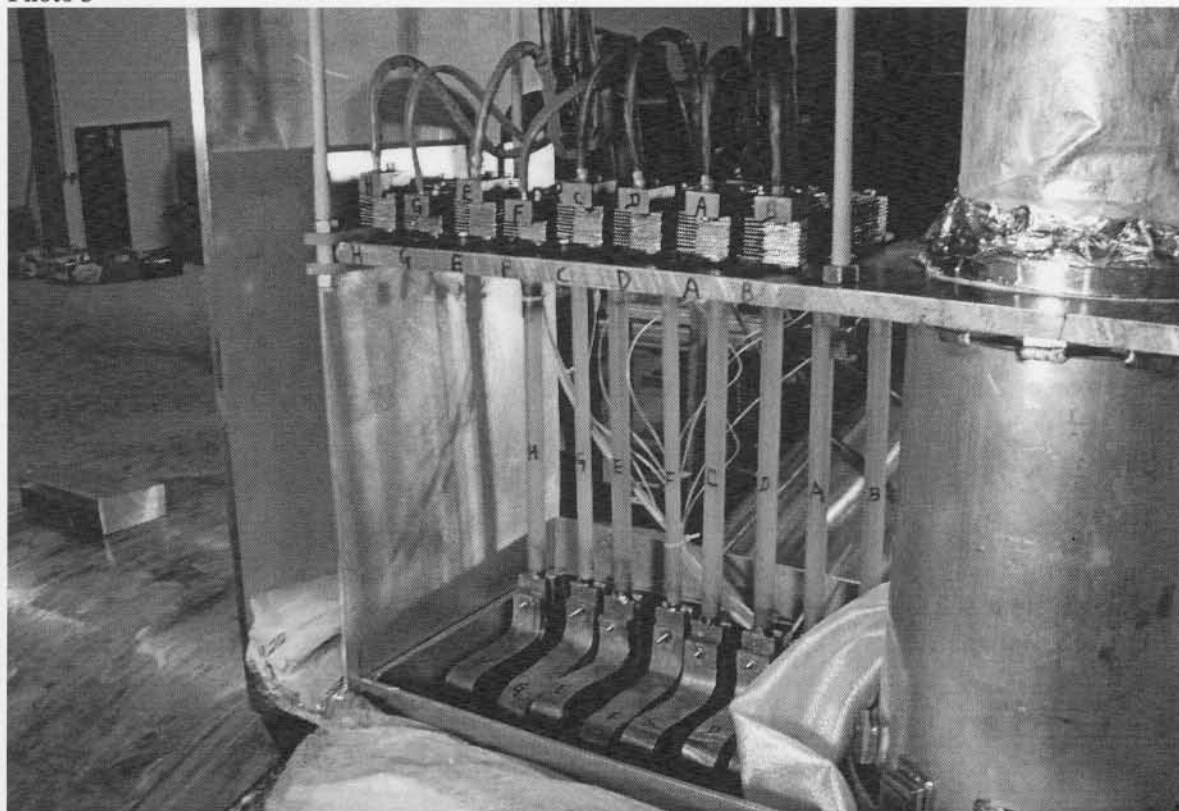
MICE COIL FABRICATION SHOWING TRACKER LONG SOLENOIDS WITH END COILS, MATCHING COILS, SUPERCONDUCTIVE FEED THROUGHS AND MAGNET PROTECTION ASSEMBLY AND HELIUM SHELL ASSEMBLY

Photo 2



CRYOSTAT FABRICATION AND ASSEMBLY

Photo 3



**SERVICE TOWER ASSEMBLY SHOWING HiTc LEADS,
HEATSINKS AND ONE OF THREE COLDHEAD ASSEMBLY**