

Gas system calculations DRAFT

Pressures for use at LBNL

Maximum Operating Pressure

$$P_{MOP} := 300\text{psi}$$

Maximum Allowable Working Pressure

$$P_{MAWP} := 350\text{psi}$$

Stored Energy, U, @ 350 psig MAWP

from PUB3000 , Chapter 7, Appendix E:

$$U = \frac{P_h V_h}{\gamma - 1} \left[1 - \left(\frac{P_1}{P_h} \right)^{\frac{\gamma-1}{\gamma}} \right]$$

where:

$$P_h := P_{MAWP} + 14.7\text{psi} \quad P_h = 364.7\text{psi} \quad P_1 := 14.7\text{psi} \quad \gamma := 1.666 \quad (\text{for monatomic gases})$$

System Volume includes vessel, cabling octagon, connection spool, recovery bottle, valve and gas system tubing:

$d_{ves} := 7.63\text{in}$	$l_{ves} := 13.5\text{in}$	main vessel inner dimensions
$d_{LNxt} := 2\text{in}$	$l_{LNxt} := 8\text{in}$	LN2 extension (cold probe)
$d_{oct} := 8\text{in}$	$l_{oct} := 3.0\text{in}$	Kimball octagon for cabling
$d_{spool} := 2\text{in}$	$l_{spool} := 10\text{in}$	connection spool, lid to octagon
$d_{tubing} := 0.5\text{in}$	$l_{tubing} := 20\text{ft}$	gas system tubing and filters
$d_{valve} := 2\text{in}$	$l_{valve} := 4\text{in}$	high pressure volume of closed valve and tank stub
$d_{rb} := 4.0\text{in}$	$l_{rb} := 36\text{in}$	recovery bottle (condensation bottle)

$$V_h := \frac{\pi}{4} \cdot (d_{ves}^2 \cdot l_{ves} + d_{LNxt}^2 \cdot l_{LNxt} + d_{spool}^2 \cdot l_{spool} + d_{oct}^2 \cdot l_{oct} + d_{tubing}^2 \cdot l_{tubing} + d_{valve}^2 \cdot l_{valve} + d_{rb}^2 \cdot l_{rb})$$

$$V_h = 1.3 \times 10^3 \text{in}^3 \quad V_h = 21.9 \text{L}$$

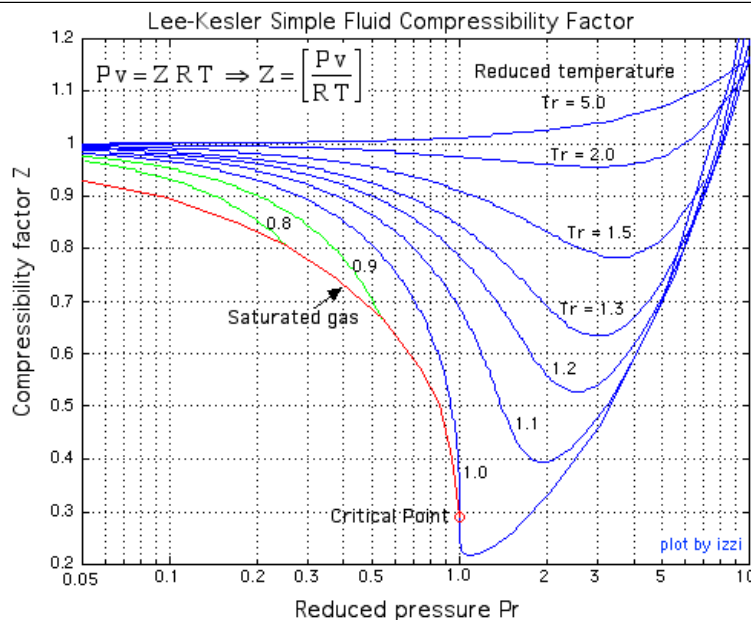
Stored Energy @ 350 psig MAWP:

$$U_v := \frac{P_h \cdot V_h}{\gamma - 1} \left[1 - \left(\frac{P_1}{P_h} \right)^{\frac{\gamma-1}{\gamma}} \right] \quad U_v = 60 \text{kJ}$$

Mass of Xenon in System at operating pressure

$$P_{MOP} = 300\text{psi} \quad R := 8.314 \text{J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1} \quad T_{amb} := 300\text{K} \quad M_{a_Xe} := 131.3 \text{gm} \cdot \text{mol}^{-1}$$

For real gases especially those that deviate strongly from ideal behavior the ideal gas law is modified with a compressibility factor Z (where v in chart below is molar density = V/n). For pure gasses (not mixtures) this factor is identical for different compounds when pressure and temperature are expressed in terms of a reduced pressure and temperature (principle of corresponding states), and can be easily found according to the following chart:



ref: A Generalized Thermodynamic Correlation based on Three-Parameter Corresponding States, B.I.Lee & M.G.Kesler, AIChE Journal, Volume 21, Issue 3, 1975, pp. 510-527' (secondary ref.
from: <http://www.ent.ohiou.edu/~thermo/>

where the reduced pressure and temperature are defined in terms of the critical pressure and temperature respectively:

Critical Pressure, Critical Temperature of Xenon:

$$P_{c_Xe} := 58.40 \text{ bar} \quad T_{c_Xe} := 15.6 \text{ K} + 273 \text{ K}$$

reduced pressure, temperature at operating condition:

$$P_r := \frac{315 \text{ psi}}{P_{c_Xe}} \quad P_r = 0.361 \quad T_r := \frac{T_{amb}}{T_{c_Xe}} \quad T_r = 1.04$$

Compressibility Factor: from chart above:

$$Z_{Xe_20\text{bar}} := 0.88$$

Number of moles:

$$n_{Xe} := \frac{P_{MOP} \cdot V_h}{Z_{Xe_20\text{bar}} \cdot R \cdot T_{amb}} \quad n_{Xe} = 20.642 \text{ mol} \quad \rho_{mol} := \frac{n_{Xe}}{V_h} \quad \rho_{mol} = 0.942 \frac{\text{mol}}{\text{L}}$$

Weight:

$$W_{Xe} := M_{a_Xe} \cdot n_{Xe} \quad W_{Xe} = 2.71 \text{ kg}$$

Volume of LXe

$$\text{density: } \rho_{LXe} := 3.05 \frac{\text{gm}}{\text{mL}} \quad @ \text{ boiling, 1 bar, } -101.8 \text{ C}$$

$$V_{LXe} := \frac{W_{Xe}}{\rho_{LXe}} \quad V_{LXe} = 0.889 \text{ L}$$

Pressure in recovery bottle

Recovery Bottle volume:

$$V_{rb} := \frac{\pi \cdot d_{rb}^2 \cdot l_{rb}}{4} \quad V_{rb} = 7.413 \text{ L}$$

we need a starting guess for pressure to iterate to find Z

$$P_{rb_guess} := 2.5 \cdot P_{MOP} \quad P_{rb_guess} = 50.2 \text{ bar}$$

then reduced pressure, temperature:

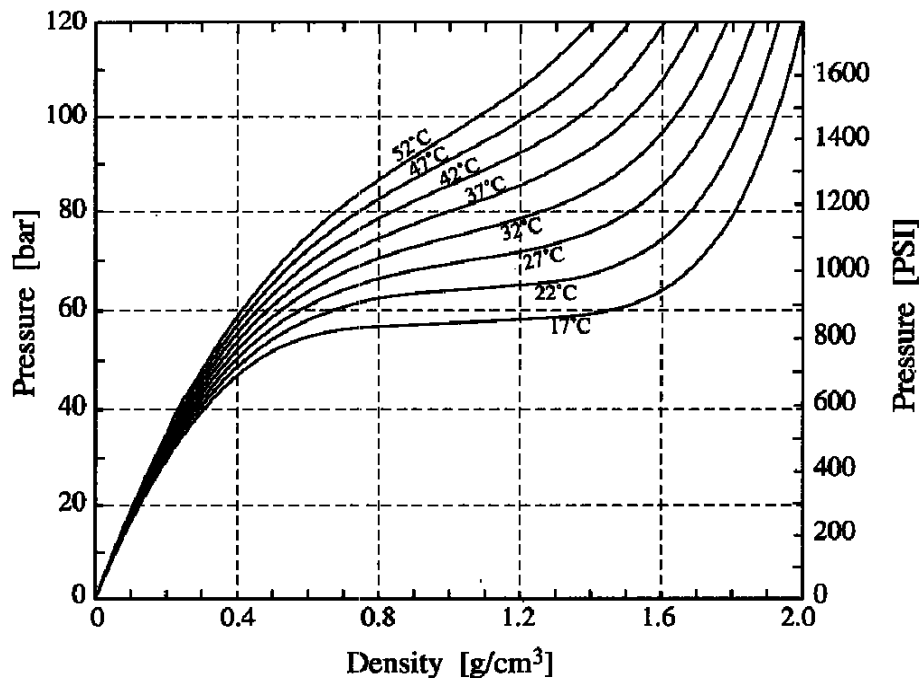
$$P_{r_rb} := \frac{P_{rb_guess}}{P_{c_Xe}} \quad P_{r_rb} = 0.86 \quad T_{hot} := (273 + 50)K \quad T_{r_hot} := \frac{T_{hot}}{T_{c_Xe}} \quad T_{r_hot} = 1.12$$

we find from chart:

$$Z_{Xe_rb_press} := .76$$

$$P_{rb} := \frac{n_{Xe} \cdot Z_{Xe_rb_press} \cdot R \cdot T_{amb}}{V_{rb}} \quad P_{rb} = 51.2 \text{ bar} \quad P_{rb} = 766 \text{ psi} \quad \text{close enough to guess}$$

Alternately, we can use a pressure density curve:



ref : A Portable Gamma Ray Spectrometer using Compressed Xenon
Mahler, IEEE Trans. Nuc. Sci. 45(3) p. 1029(1998)

for mass density

$$\rho_{mass_rb} := \rho_{mol_rb} \cdot M_{a_Xe} \quad \rho_{mass_rb} = 0.366 \frac{\text{gm}}{\text{cm}^3}$$

we find a maximum pressure of

$$P_{max_rb} := 55 \text{ bar} \quad P_{max_rb} = 822 \text{ psi} \quad \text{at } 50^\circ\text{C, which is the maximum temperature we expect to see. The gas filters have a maximum temperature of } 40^\circ\text{C.}$$