

Mesh Deflection

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Operating parameters

frame radius

$$p := 15 \text{ bar} \quad E_{\text{ovrP}} := 4 \frac{\text{kV}}{\text{cm} \cdot \text{bar}} \quad E_{\text{EL}} := E_{\text{ovrP}} \cdot p \quad E_{\text{EL}} = 60 \frac{\text{kV}}{\text{cm}} \quad E_{\text{dr}} := 1 \frac{\text{kV}}{\text{cm}} \quad R_{\text{mp}} := 51 \text{ cm}$$

gap

Voltage

$$d_{\text{EL}} := 10 \text{ mm} \quad V_{\text{EL}} := d_{\text{EL}} \cdot E_{\text{EL}} \quad V_{\text{EL}} = 6 \times 10^4 \text{ V}$$

Mesh modulus: assume no wire crossing; isotropic properties

open area fraction

$$\begin{array}{lll} \text{mesh wire dia} & \text{wire spacing} & \text{wire elastic modulus} \\ d_{\text{mw}} := .009 \text{ in} & s_{\text{mw}} := \frac{1}{14} \text{ in} & E_{\text{ss}} := 28 \cdot 10^6 \text{ psi} \quad E_{\text{ss}} = 193 \text{ GPa} \end{array}$$

$$\eta_a := \frac{(s_{\text{mw}} - d_{\text{mw}})^2}{s_{\text{mw}}^2} \quad \eta_a = 76 \%$$



equivalent mesh elastic modulus will be material modulus * cross section areal fill ratio

$$N_a := \frac{\frac{\pi}{4} d_{\text{mw}}^2}{s_{\text{mw}} \cdot d_{\text{mw}}} \quad N_a = 0.099$$

$$E_{\text{mesh}} := E_{\text{ss}} N_a \quad E_{\text{mesh}} = 19.1 \text{ GPa}$$

Pressure, from electric field (EL -drift field) (ignore gravity for dual mesh planes)

$$P_{\text{EL}} := 0.5 \epsilon_0 (E_{\text{EL}} - E_{\text{dr}})^2 \quad P_{\text{EL}} = 154 \text{ Pa}$$

Large Deflection Formula for Circular Membrane with initial stress under pressure loading:

deflection is primarily a function of initial stress condition (prestress)

reference: A New Analytical Solution for Diaphragm Deflection and its Application to a Surface Micromachined Pressure Sensor. W.P.Eaton, et. al:

let equivalent mesh prestress be:

S.S Ultimate Strength

$$\sigma_{\text{ps}} := 0.75 S_{\text{u_ss}} \cdot N_a \quad \sigma_{\text{ps}} = 38.38 \text{ MPa}$$

$$S_{\text{u_ss}} := 75000 \text{ psi} \quad S_{\text{u_ss}} = 517.1 \text{ MPa}$$

let:

Poisson's ratio

$$h := d_{\text{mw}} \quad a := R_{\text{mp}} \quad E := E_{\text{mesh}} \quad P := P_{\text{EL}}$$

$$\nu := \frac{d_{\text{mw}}}{s_{\text{mw}}} \quad \nu = 0.126$$

Poisson's ratio is given only for free transverse boundary, so for mesh it will depend only on wire dia and spacing (probably $\nu = \theta$):

Initial strain:

$$\epsilon_i := \frac{\sigma_{\text{ps}}}{E_{\text{mesh}}} \quad \epsilon_i = 0.201 \%$$

Plate constant:

$$d_{\text{mw}} = 2.286 \times 10^{-4} \text{ m}$$

$$D := \frac{E \cdot h^3}{12(1 - \nu^2)} \quad D = 0.019 \text{ N} \cdot \text{m}$$

ref. eqs 3

compute the following:

$$\alpha := 14 \cdot \frac{(2 \cdot h)^2 + 3a^2 \cdot \epsilon_1 \cdot (1 + \nu)}{(1 + \nu) \cdot (23 - 9\nu)} \quad \alpha = 1.004 \times 10^{-3} \text{ m}^2 \quad \text{ref. eqs 17}$$

$$\beta := -7P \cdot a^4 \frac{h^2}{8D \cdot (1 + \nu) \cdot (23 - 9\nu)} \quad \beta = -1.001 \times 10^{-6} \text{ m}^3 \quad \text{ref. eqs 17}$$

$$\gamma := \sqrt{\frac{\alpha^3}{27} + \frac{\beta^2}{4}} \quad \gamma = 6.141 \times 10^{-6} \text{ m}^3 \quad \text{ref. eqs 17}$$



deflection is:

percentage gap decrease

$$f := \sqrt[3]{\frac{-\beta}{2} + \gamma} + \sqrt[3]{\frac{-\beta}{2} - \gamma} \quad f = 0.997 \text{ mm} \quad \frac{2f}{d_{EL}} = 19.9 \% \quad \text{ref. eqs 17}$$