

Mass of Xenon in Vessel at Maximum Operating Pressure (absolute):

Assume we have 100 kg Xe in active volume of gas inside a cylinder inscribed within the field cage (TTX panels)

$$M_{Xe\_100} := 100\text{kg}$$

Maximum Operating pressure (absolute):

$$P_{MOPa\_100} := 15\text{bar}$$

Minimum Operating pressure (minus sign indicates external pressure)

$$P_{min} := -1.5\text{bar}$$

this is driven by the need to pull vacuum with a possible hydrostatic head of 0.4bar if water tank is used for shielding

Operating Temperature, physical constants:

$$T_{amb} := 293\text{K}$$

$$R := 8.314\text{J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$$

$$M_{a\_Xe} := 136\text{gm}\cdot\text{mol}^{-1}$$

Critical Pressure, temperature of Xenon:

$$P_{c\_Xe} := 58.40\text{bar} \quad T_{c\_Xe} := 15.6\text{K} + 273\text{K} \quad T_{c\_Xe} = 288.6\text{K}$$

reduced pressure:

$$P_{r\_100} := \frac{P_{MOPa\_100}}{P_{c\_Xe}} \quad P_{r\_100} = 0.257 \quad P_{r\_8bar} := \frac{8\text{bar}}{P_{c\_Xe}} \quad P_{r\_8bar} = 0.137$$

reduced temperature

$$T_r := \frac{T_{amb}}{T_{c\_Xe}} \quad T_r = 1.015$$

Compressibility Factor: from chart for pure gasses shown below

$$Z_{Xe\_15bar} := .93$$

$$Z_{Xe\_8bar} := .96$$

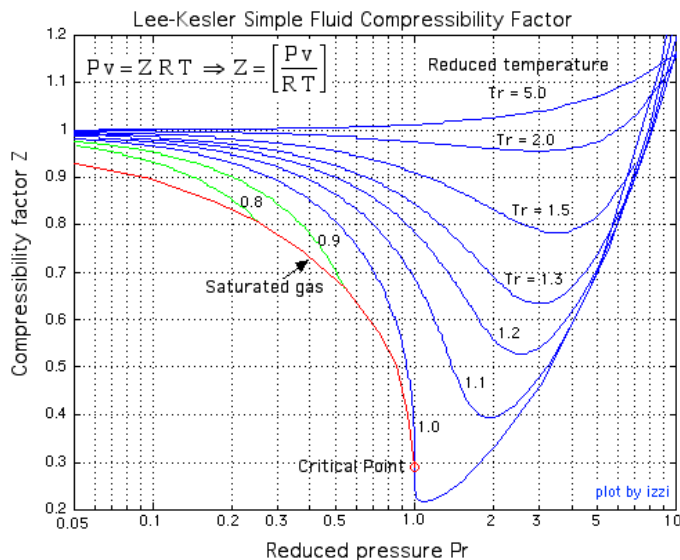


Fig. 6 Compressibility Factor, pure gasses

Number of moles:

$$n_{Xe\_100} := \frac{M_{Xe\_100}}{M_{a\_Xe}} \quad n_{Xe\_100} = 735.294\text{ mol}$$

Current vessel interior volume is 2.0 m<sup>3</sup> ( vessel vol. - internal component vols). If we have 100kg total Xe then operating pressure is:

ref: A Generalized Thermodynamic Correlation based on Three-Parameter Corresponding States, B.I.Lee & M.G.Kesler, AIChE Journal, Volume 21, Issue 3, 1975, pp. 510-527' (secondary ref. from: <http://www.ent.ohiou.edu/~t-hermo/>)

$$P_{100\text{kg\_tot}} := \frac{n_{\text{Xe}_100} \cdot Z_{\text{Xe}_8\text{bar}} \cdot R \cdot T_{\text{amb}}}{2\text{m}^3} \quad P_{100\text{kg\_tot}} = 8.483 \text{ bar}$$

Volume required:

$$V_{\text{Xe}_100} := \frac{n_{\text{Xe}_100} \cdot Z_{\text{Xe}_15\text{bar}} \cdot R \cdot T_{\text{amb}}}{P_{\text{MOPa}_100}} \quad V_{\text{Xe}_100} = 1.096 \text{ m}^3$$

$$n_{\text{Xe}} := n_{\text{Xe}_100} \quad V_{\text{Xe}} := V_{\text{Xe}_100} \quad P_{\text{MOPa}} := P_{\text{MOPa}_100}$$

molar, mass, volumetric density:

$$\rho_{\text{mol}} := \frac{n_{\text{Xe}}}{V_{\text{Xe}}} \quad \rho_{\text{mol}} = 0.671 \frac{\text{mol}}{\text{L}}$$

$$\rho_{\text{Xe}} := \rho_{\text{mol}} \cdot M_{\text{a\_Xe}} \quad \rho_{\text{Xe}} = 0.091 \frac{\text{gm}}{\text{cm}^3}$$

$$v_{\text{Xe}} := \rho_{\text{Xe}}^{-1} \quad v_{\text{Xe}} = 10.957 \frac{\text{cm}}{\text{gm}}$$

$$P_{\text{h}} := 1.15 P_{\text{MOPa}} \quad \gamma := 1.666$$

$$P_{\text{l}} := 1 \text{ bar} \quad V_{\text{h}} := 1.5 V_{\text{Xe}}$$

Stored Energy @ 15.4 bar MOP

$$U_{\text{v}} := \frac{P_{\text{h}} \cdot V_{\text{h}}}{\gamma - 1} \left[ 1 - \left( \frac{P_{\text{l}}}{P_{\text{h}}} \right)^{\frac{\gamma-1}{\gamma}} \right] \quad U_{\text{v}} = 2.9 \text{ MJ}$$

We desire active length to be = 1.25x active diameter. then:

$$\text{Active volume radius: } r_{\text{Xe\_exact}} := \sqrt[3]{\frac{V_{\text{Xe}}}{2.5\pi}} \quad r_{\text{Xe\_exact}} = 0.5186425 \text{ m}$$

$$\text{then: } l_{\text{Xe\_exact}} := 2.5 r_{\text{Xe\_exact}} \quad l_{\text{Xe\_exact}} = 1.296606 \text{ m}$$

Round up to:

$$r_{\text{Xe}} := 0.53 \text{ m} \quad l_{\text{Xe}} := 1.30 \text{ m} \quad \pi r_{\text{Xe}}^2 \cdot l_{\text{Xe}} = 1.147 \text{ m}^3$$

Field Cage Ring minor radius

$$r_{\text{fc\_minor}} := 0.5 \text{ cm}$$

## Pressure Vessel Design Calculations, DRAFT Stainless steel vessel with Copper Liner D. Shuman, Nov 3,/2011

Active volume dimensions, from earlier analyses:

$$r_{Xe} = 0.53 \text{ m} \quad l_{Xe} = 1.3 \text{ m}$$

We consider using a field cage solid insulator/light tube of 2 cm thk. and a copper liner of 6 cm thickness

$$t_{fc} := 3 \text{ cm} \quad t_{Cu} := 12 \text{ cm} \quad \text{note: copper will be notched at internal flange}$$

Pressure Vessel inner radius is then:

$$R_{i\_pv} := r_{Xe} + t_{fc} + t_{Cu} \quad R_{i\_pv} = 0.68 \text{ m}$$

### Vessel wall thicknesses DRAFT

Pressure vessel inner radius:  $R_{i\_pv} = 68 \text{ cm}$

We choose to use division 2 rules, which allow thinner walls at the expense of performing more strict material acceptance and additional NDE post weld inspection, as we will be performing these steps regardless, due to the high value of the vessel contents. For flat-faced flanges we use div. 1, as no methodology exists in div 2. Div. 1 is more typically conservative than div. 2, when div. 2 quality control is implemented.

Maximum allowable material stresses, for sec VIII, division 2 rules from ASME 2009 Pressure Vessel code, sec. II part D, table 5B (div. 1 stress from table 1A):

Youngs modulus

$$S_{\max\_304L\_div2} := 16700 \text{ psi} \quad S_{\max\_304L\_div1} := 16700 \text{ psi} \quad E_{SS\_aus} := 193 \text{ GPa}$$

$$S_{\max\_316L\_div2} := 16700 \text{ psi} \quad S_{\max\_316L\_div1} := 16700 \text{ psi} \quad \text{we use the L grades for weldability}$$

### color scheme for this document

input    check result (all conditions should be true (=1))

$$xx := 1 \quad xx > 0 = 1$$

Choose material:

$$S_{\max} := S_{\max\_304L\_div2}$$

Maximum Operating Pressure (MOP), gauge:

$$MOP_{pv} := (P_{MOPa} - 1 \text{ bar}) \quad MOP_{pv} = 14 \text{ bar}$$

Minimum Pressure, gauge:

$$P_{\min} = -1.5 \text{ bar} \quad \text{the extra 0.5 atm maintains an upgrade path to a water or scintillator tank}$$

Maximum allowable pressure, gauge (from LBNL Pressure Safety Manual, PUB3000)  
at a minimum, 15% over max operating pressure; this is design pressure at LBNL:

$$MAWP_{pv} := 1.1 MOP_{pv} \quad MAWP_{pv} = 15.4 \text{ bar}$$

Vessel wall thickness, for internal pressure is then ( div 2):

$$t_{pv\_d2\_min\_ip} := R_{i\_pv} \cdot \left( e^{\frac{MAWP_{pv}}{S_{\max}}} - 1 \right) \quad t_{pv\_d2\_min\_ip} = 9.281 \text{ mm}$$

Compare with div. 1 rules ( weld efficiency  $E=1$ )  $E_w := 1$

$$t_{pv\_d1\_min\_ip} := \frac{MAWP_{pv} \cdot (R_{i\_pv})}{S_{\max\_304L\_div1} \cdot E_w - 0.6 \cdot MAWP_{pv}} \quad t_{pv\_d1\_min\_ip} = 9.293 \text{ mm}$$

There seems to be little difference between using division 1 or 2 for a 304L stainless steel vessel. We continue with div 2 rules, since we have high quality assurance standards anyway. We set wall thickness to be:

$$t_{pv} := 10\text{mm}$$

$$t_{pv} > t_{pv\_d2\_min\_ip} = 1$$

### Maximum Allowable External pressure using ASME PV code Sec. VIII div 2 rules, 4.4.5

Step 1- trial thickness, outer radius, diameter longest length between flanges:

$$R_{O\_pv} := R_{i\_pv} + t_{pv} \quad D_o := 2R_{O\_pv} \quad L_{ff} := 1.52\text{m}$$

material elastic modulus:

$$E_y := E_{SS\_aus} \quad E_y = 193\text{ GPa}$$

Step 2 compute the following:

or greater

$$M_x := \frac{L_{ff}}{\sqrt{R_{O\_pv} \cdot t_{pv}}} \quad M_x = 18.299 \quad S_{y\_Ti\_g2} := 40000\text{psi}$$

$$\text{for} \quad 2 \left( \frac{D_o}{t_{pv}} \right)^{.94} = 205.36 \quad S_y := S_{y\_Ti\_g2}$$

$$C_h := 1.12 M_x^{-1.058} \quad C_h = 0.052$$

$$F_{he} := \frac{1.6 \cdot C_h \cdot E_y \cdot t_{pv}}{2(D_o)} \quad F_{he} = 57.856\text{ MPa} \quad \frac{F_{he}}{S_y} = 0.21$$

$$F_{ic} := F_{he}$$

$$\frac{F_{he}}{S_y} \leq .552 = 1$$

$$F_{ha} := \frac{F_{ic}}{2} \quad \text{per 4.4.2 eq. (4.4.1)}$$

$$FS := 2 \quad P_{a\_div2} := 2F_{ha} \cdot \left( \frac{t_{pv}}{D_o} \right) \quad P_{a\_div2} = 4.136\text{ bar} \quad P_{a\_div2} > -P_{min} = 1$$

### Flange thickness:

inner radius	max. allowable pressure
$R_{i\_pv} = 0.68\text{ m}$	$MAWP_{pv} = 15.4\text{ bar}$ (gauge pressure)

The flange design for heliocflex or O-ring sealing is "flat-faced", with "metal to metal contact outside the bolt circle". This design avoids the high flange bending stresses found in a raised face flange (of Appendix 2) and will result in less flange thickness, even though the rules for this design are found only in sec VIII division 1 under Appendix Y, and must be used with the lower allowable stresses of division 1.

Flanges and shells will be fabricated from 304L or 316L (ASME spec SA-240) stainless steel plate. Plate samples will be helium leak checked before fabrication, as well as ultrasound inspected. The flange bolts and nuts will be inconel 718, (UNS N77180) as this is the highest strength non-corrosive material allowed for bolting.

We will design to use one Heliocflex 5mm gasket (smallest size possible) with aluminum facing (softest) loaded to the minimum force required to achieve helium leak rate.

Maximum allowable material stresses, for sec VIII, division 1 rules from ASME 2010 Pressure Vessel code, sec. II part D, table 2B:

Maximum allowable design stress for flange

$$S_f := S_{\max\_304L\_div1} \quad S_f = 115.1 \text{ MPa}$$

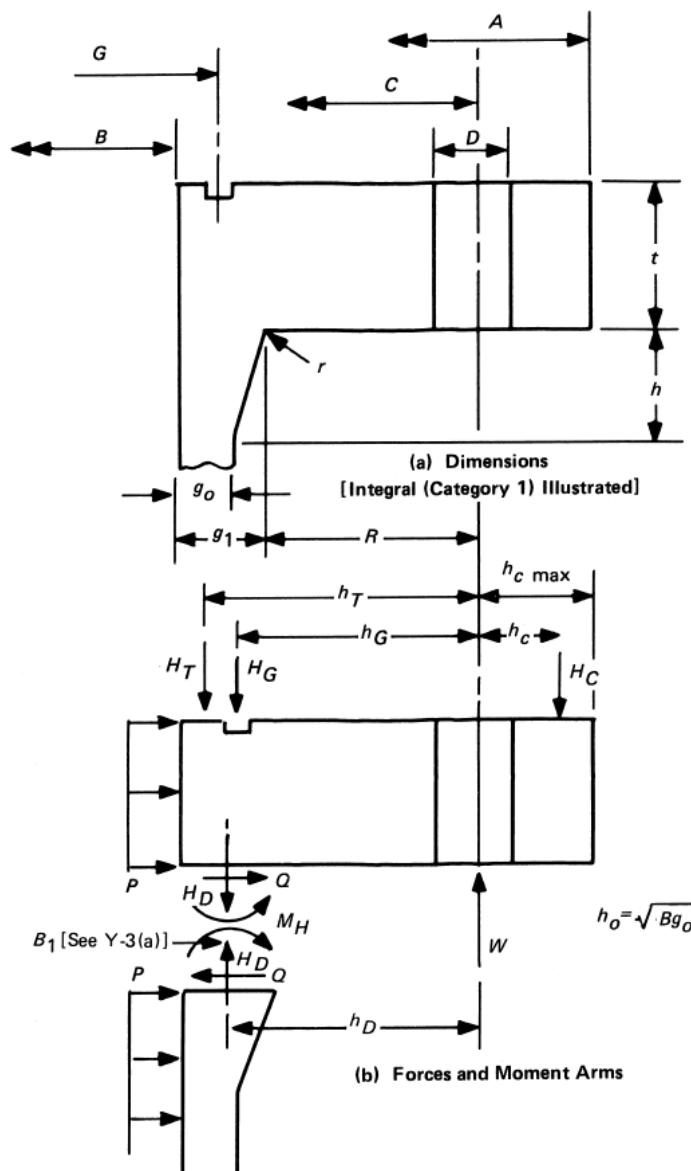
Maximum allowable design stress for bolts, from ASME 2010 Pressure Vessel code, sec. II part D, table 3

$$\text{Inconel 718 (UNS N07718)} \quad S_{\max\_N07718} := 37000 \text{ psi}$$

$$S_b := S_{\max\_N07718} \quad S_b = 255.1 \text{ MPa}$$

From sec. VIII div 1, non-mandatory appendix Y for bolted joints having metal-to-metal contact outside of bolt circle. First define, per Y-3:

FIG. Y-3.2 FLANGE DIMENSIONS AND FORCES



hub thickness at flange (no hub)

corner radius:

$$g_0 := t_{pv} \quad g_1 := t_{pv} \quad g_0 = 10 \text{ mm} \quad g_1 = 10 \text{ mm} \quad r_1 := \max(.25g_1, 5 \text{ mm}) \quad r_1 = 5 \text{ mm}$$

Flange OD

$$A := 1.47 \text{ m}$$

Flange ID

$$B := 2R_{i\_pv} \quad B = 1.36 \text{ m}$$

define:

$$B_1 := B + g_1 \quad B_1 = 1.37 \text{ m}$$

Bolt circle (B.C.) dia, C:

$$C := 1.43 \text{ m}$$

Gasket dia

$$G := 2(R_{i\_pv} + .75 \text{ cm}) \quad G = 1.375 \text{ m}$$

Force of Pressure on head

$$H := .785 G^2 \cdot \text{MAWP}_{pv} \quad H = 2.316 \times 10^6 \text{ N}$$

Sealing force, per unit length of circumference:

for O-ring, 0.275" dia., shore A 70  $F = \sim 5$  lbs/in for 20% compression, (Parker o-ring handbook); add 50% for smaller second O-ring. (Helicoflex gasket requires high compression, may damage soft Ti surfaces, may move under pressure unless tightly backed, not recommended)

Helicoflex has equivalent values  $Y$  for the force time and gives several possible values for 5mm HN200 with aluminum jacket:

$$Y_1 := 30 \frac{\text{N}}{\text{mm}} \quad \text{min value for our pressure and required leak rate (He)} \quad Y_2 := 150 \frac{\text{N}}{\text{mm}} \quad \text{recommended value for large diameter seals, regardless of pressure or leak rate}$$

$$\text{for gasket diameter} \quad D_j := G \quad D_j = 1.375 \text{ m}$$

Force is then either of:

$$F_m := 2\pi D_j \cdot Y_1 \quad \text{or} \quad F_j := 2\pi D_j \cdot Y_2$$
$$F_m = 2.592 \times 10^5 \text{ N} \quad F_j = 1.296 \times 10^6 \text{ N}$$

Helicoflex recommends using  $Y_2$  (220 N/mm) for large diameter seals, even though for small diameter one can use the greater of  $Y_1$  or  $Y_m = (Y_2 \cdot (P/P_u))$ . For 15 bar  $Y_1$  is greater than  $Y_m$  but far smaller than  $Y_2$ . Sealing is less assured, but will be used in elastic range and so may be reusable. Flange thickness and bolt load increase quite substantially when using  $Y_2$  as design basis, which is a large penalty. We plan to recover any Xe leakage, as we have a second O-ring outside the first and a sniff port in between, so we thus design for  $Y_1$  (use  $F_m$ ) and "cross our fingers": if it doesn't seal we use an O-ring instead and recover permeated Xe with a cold trap. A PCTFE O-ring may give lower permeability, but have a higher force requirement, than for a normal butyl or nitrile O-ring; designing to  $Y_1$  will account for this. Note: in the cold trap one will get water and  $N_2$ ,  $O_2$ , that permeates through the outer O-ring as well.

Start by making trial assumption for number of bolts, root dia., pitch, bolt hole dia  $D$ ,

$$n := 150 \quad d_b := 12.77 \text{ mm}$$

Choosing ISO fine thread, with pitch; thread depth:

$$p_t := 1.0 \text{ mm} \quad d_t := .614 \cdot p_t$$

Nominal bolt dia is then;

$$d_{b\_nom\_min} := d_b + 2d_t \quad d_{b\_nom\_min} = 13.998 \text{ mm}$$

Set:

$$d_{b\_nom} := 14 \text{ mm} \quad d_{b\_nom} > d_{b\_nom\_min} = 1$$

Check bolt to bolt clearance, for box wrench b2b spacing is 1.2 in for 1/2in bolt twice bolt dia (  $2.4 \times d_b$  ):

$$\pi C - 2.0n \cdot d_{b\_nom} \geq 0 = 1$$

Check nut, washer clearance:  $OD_w := 2d_{b\_nom}$  this covers the nut width across corners

$$0.5C - (0.5B + g_1 + r_1) \geq 0.5OD_w = 1$$

Flange hole diameter, minimum for clearance :

$$D_{tmin} := d_{b\_nom} + 0.5mm \quad D_{tmin} = 14.5 \text{ mm}$$

Set:

$$D_t := 15mm$$

$$D_t > D_{tmin} = 1$$

Compute Forces on flange:

$$H_G := F_m \quad H_G = 2.592 \times 10^5 \text{ N}$$

$$h_G := 0.5(C - G) \quad h_G = 2.75 \text{ cm}$$

$$H_D := .785 \cdot B^2 \cdot MAWP_{pv} \quad H_D = 2.266 \times 10^6 \text{ N}$$

$$h_D := D_t \quad h_D = 1.5 \text{ cm}$$

$$H_T := H - H_D \quad H_T = 5.027 \times 10^4 \text{ N}$$

$$h_T := 0.5(C - B) \quad h_T = 35 \text{ mm}$$

Total Moment on Flange

$$M_P := H_D \cdot h_D + H_T \cdot h_T + H_G \cdot h_G \quad M_P = 4.288 \times 10^4 \text{ J}$$

## Appendix Y Calc

$$P := MAWP_{pv} \quad P = 1.561 \times 10^6 \text{ Pa}$$

Choose values for plate thickness and bolt hole dia:

$$t := 3.5cm \quad D := D_t \quad D = 1.5 \text{ cm}$$

Going back to main analysis, compute the following quantities:

$$\beta := \frac{C + B_1}{2B_1} \quad \beta = 1.022 \quad h_C := 0.5(A - C) \quad h_C = 0.02 \text{ m}$$

$$a := \frac{A + C}{2B_1} \quad a = 1.058 \quad AR := \frac{n \cdot D}{\pi \cdot C} \quad AR = 0.501 \quad h_0 := \sqrt{B \cdot g_0}$$

$$r_B := \frac{1}{n} \left( \frac{4}{\sqrt{1 - AR^2}} \operatorname{atan} \left( \sqrt{\frac{1 + AR}{1 - AR}} \right) - \pi - 2AR \right) \quad r_B = 4.656 \times 10^{-3} \quad h_0 = 0.117 \text{ m}$$

We need factors F and G, most easily found in figs 2-7.2 and 7.3 (Appendix 2)

$$\text{since } \frac{g_1}{g_0} = 1 \quad \text{these values converge to} \quad F := 0.90892 \quad V := 0.550103$$

## Y-5 Classification and Categorization

We have identical (class 1 assembly) integral ( category 1) flanges, so from table Y-6.1, our applicable equations are (5a), (7)-(13),(14a),(15a),16a)

$$J_S := \frac{1}{B_1} \left( \frac{2 \cdot h_D}{\beta} + \frac{h_C}{a} \right) + \pi r_B \quad J_S = 0.05 \quad J_P := \frac{1}{B_1} \left( \frac{h_D}{\beta} + \frac{h_C}{a} \right) + \pi r_B \quad J_P = 0.039$$

$$(5a) \quad F' := \frac{g_0^2 (h_0 + F \cdot t)}{V} \quad F' = 2.698 \times 10^{-5} \text{ m}^3 \quad M_P = 4.288 \times 10^4 \text{ N}\cdot\text{m}$$

$$A = 1.47 \text{ m} \quad B = 1.36 \text{ m}$$

$$K := \frac{A}{B} \quad K = 1.081 \quad Z := \frac{K^2 + 1}{K^2 - 1} \quad Z = 12.883$$

$$f := 1$$

$$t_s := 0 \text{ mm} \quad \text{no spacer}$$

$$l := 2t + t_s + 0.5d_b \quad l = 7.639 \text{ cm} \quad A_b := n \cdot 785 d_b^2$$

sec Y-6.2(a)(3)

Elastic constants

<http://www.hightempmetals.com/tech-data/hitempInconel718data.php>

$$(7-13) \quad E := E_{SS\_aus} \quad E_{Inconel\_718} := 208 \text{ GPa} \quad E_{bolt} := E_{Inconel\_718}$$

$$M_S := \frac{-J_P \cdot F' \cdot M_P}{t^3 + J_S \cdot F'} \quad M_S = -1 \times 10^3 \text{ J}$$

$$\theta_B := \frac{5.46}{E \cdot \pi t^3} (J_S \cdot M_S + J_P \cdot M_P) \quad \theta_B = 3.417 \times 10^{-4} \quad E \cdot \theta_B = 65.957 \text{ MPa}$$

$$H_C := \frac{M_P + M_S}{h_C} \quad H_C = 2.093 \times 10^6 \text{ N}$$

$$W_{m1} := H + H_G + H_C \quad W_{m1} = 4.668 \times 10^6 \text{ N}$$

### Compute Flange and Bolt Stresses

$$\sigma_b := \frac{W_{m1}}{A_b} \quad \sigma_b = 243.1 \text{ MPa} \quad S_b = 255.1 \text{ MPa}$$

$$r_E := \frac{E}{E_{bolt}} \quad r_E = 0.928$$

$$S_i := \sigma_b - \frac{1.159 \cdot h_C^2 \cdot (M_P + M_S)}{a \cdot t^3 \cdot 1 \cdot r_E \cdot B_1} \quad S_i = 238.7 \text{ MPa}$$

$$S_{R\_BC} := \frac{6(M_P + M_S)}{t^2 (\pi \cdot C - n \cdot D)} \quad S_{R\_BC} = 91.4 \text{ MPa} \quad S_f = 115.1 \text{ MPa}$$

$$S_{R\_ID1} := - \left( \frac{2F \cdot t}{h_0 + F \cdot t} + 6 \right) \cdot \frac{M_S}{\pi B_1 \cdot t^2} \quad S_{R\_ID1} = 1.249 \text{ MPa}$$



$$S_{T1} := \frac{t \cdot E \cdot \theta_B}{B_1} + \left( \frac{2F \cdot t \cdot Z}{h_0 + F \cdot t} - 1.8 \right) \cdot \frac{M_S}{\pi B_1 \cdot t^2} \quad S_{T1} = 0.96 \text{ MPa}$$

$$S_{T3} := \frac{t \cdot E \cdot \theta_B}{B_1} \quad S_{T3} = 1.685 \text{ MPa}$$

$$S_H := \frac{h_0 \cdot E \cdot \theta_B \cdot f}{0.91 \left( \frac{g_1}{g_0} \right)^2 B_1 \cdot V} \quad S_H = 11.216 \text{ MPa}$$

**Y-7 Flange stress allowables:**  $S_f = 115.1 \text{ MPa}$

(a)  $\sigma_b < S_b = 1$

(b) (1)  $S_H < 1.5S_f = 1$   $S_n$  not applicable

(2) not applicable

(c)  $S_{R\_BC} < S_f = 1$   
 $S_{R\_ID1} < S_f = 1$

(d)  $S_{T1} < S_f = 1$   
 $S_{T3} < S_f = 1$

(e)  $\frac{S_H + S_{R\_BC}}{2} < S_f = 1$   
 $\frac{S_H + S_{R\_ID1}}{2} < S_f = 1$

(f) not applicable

Shear stress in inner flange lip from shield

$$M_{sh} := 4000 \text{ kg} \quad t_{lip} := 3 \text{ mm}$$

$$\tau_{lip} := \frac{M_{sh} \cdot g}{R_{i\_pv} \cdot t_{lip}} \quad \tau_{lip} = 19.229 \text{ MPa}$$

Shear stress on O-ring land (section between inner and outer O-ring)

$$t_{land\_radial} := .36 \text{ cm} \quad w_{land\_axial} := .41 \text{ cm}$$

$$F_{O\_ring\_land} := 2\pi R_{i\_pv} \cdot w_{land\_axial} \cdot P$$

$$A_{O\_ring\_land} := 2\pi R_{i\_pv} \cdot t_{land\_radial}$$

$$\tau_{land} := \frac{F_{O\_ring\_land}}{A_{O\_ring\_land}} \quad \tau_{land} = 1.778 \text{ MPa}$$

Bolt force

$$F_{bolt} := \sigma_b \cdot .785 \cdot d_b^2 \quad F_{bolt} = 6.997 \times 10^3 \text{ lbf}$$

Bolt torque required

$$T_{\text{bolt\_min}} := 0.2 F_{\text{bolt}} \cdot d_b$$

$$T_{\text{bolt\_min}} = 79.5 \text{ N}\cdot\text{m}$$

$$T_{\text{bolt\_min}} = 58.6 \text{ lbf}\cdot\text{ft}$$

for pressure test use 1.5x  
this value

**ANGEL Torispheric Head Design, using (2010 ASME PV Code Section VIII, div. 2, part 4 rules)****2 nozzle head using standard dimension head****DRAFT**

D. Shuman, LBNL, July12, 2011

4.3.6.1 Torispheric head with same crown and knuckle thickness standard dimensions.

(a) Step 1, determine I.D. and assume the following:

thickness:

$$t_{ts} := t_{pv} \quad t_{ts} = 1 \text{ cm}$$

I.D.

$$D_i := 2R_{i\_pv}$$

O.D.

$$D := D_i + 2t_{ts} \quad D = 1.38 \text{ m}$$

Crown radius:

Knuckle radius:

$$L_{cr} := 1D_i \quad L_{cr} = 1.36 \text{ m} \quad r_{kn} := 0.1D_i \quad r_{kn} = 0.136 \text{ m}$$

(b) Step 2- Compute the following ratios and check:

$$0.7 \leq \frac{L_{cr}}{D_i} \leq 1.0 = 1$$

$$\frac{r_{kn}}{D_i} \geq 0.06 = 1$$

$$20 \leq \frac{L_{cr}}{t_{ts}} \leq 2000 = 1$$

for all true, continue, otherwise design using part 5 rules

(c) Step 3 calculate:

thickness, this is an iterated value after going through part 4.5.10.1 (openings) further down in the document

$$\beta_{th} := \arccos\left(\frac{0.5D_i - r_{kn}}{L_{cr} - r_{kn}}\right) \quad \beta_{th} = 1.11 \text{ rad}$$

$$\phi_{th} := \frac{\sqrt{L_{cr} \cdot t_{ts}}}{r_{kn}} \quad \phi_{th} = 0.857 \text{ rad}$$

$$R_{th} := \begin{cases} \frac{0.5D_i - r_{kn}}{\cos(\beta_{th} - \phi_{th})} + r_{kn} & \text{if } \phi_{th} < \beta_{th} \\ 0.5D_i & \text{if } \phi_{th} \geq \beta_{th} \end{cases} \quad \begin{matrix} \phi_{th} < \beta_{th} = 1 \\ \phi_{th} \geq \beta_{th} = 0 \end{matrix}$$

$$R_{th} = 0.698 \text{ m}$$

(d) Step 4 compute:

$$C_{1ts} := \begin{cases} \left[ 9.31 \left( \frac{r_{kn}}{D_i} \right) - 0.086 \right] & \text{if } \frac{r_{kn}}{D_i} \leq 0.08 \\ \left[ 0.692 \left( \frac{r_{kn}}{D_i} \right) + 0.605 \right] & \text{if } \frac{r_{kn}}{D_i} > 0.08 \end{cases} \quad \begin{matrix} \frac{r_{kn}}{D_i} \leq 0.08 = 0 \\ \frac{r_{kn}}{D_i} > 0.08 = 1 \end{matrix} \quad (4.3.12)$$

$$C_{1ts} := \begin{cases} \left[ 9.31 \left( \frac{r_{kn}}{D_i} \right) - 0.086 \right] & \text{if } \frac{r_{kn}}{D_i} \leq 0.08 \\ \left[ 0.692 \left( \frac{r_{kn}}{D_i} \right) + 0.605 \right] & \text{if } \frac{r_{kn}}{D_i} > 0.08 \end{cases} \quad \begin{matrix} \frac{r_{kn}}{D_i} \leq 0.08 = 0 \\ \frac{r_{kn}}{D_i} > 0.08 = 1 \end{matrix} \quad (4.3.13)$$

$$C_{1ts} = 0.674$$

$$C_{2ts} := \begin{cases} 1.25 & \text{if } \frac{r_{kn}}{D_i} \leq 0.08 \\ 1.46 - 2.6 \cdot \left( \frac{r_{kn}}{D_i} \right) & \text{if } \frac{r_{kn}}{D_i} > 0.08 \end{cases} \quad \begin{matrix} \frac{r_{kn}}{D_i} \leq 0.08 = 0 \\ \frac{r_{kn}}{D_i} > 0.08 = 1 \end{matrix} \quad (4.3.14)$$

$$C_{2ts} := \begin{cases} 1.25 & \text{if } \frac{r_{kn}}{D_i} \leq 0.08 \\ 1.46 - 2.6 \cdot \left( \frac{r_{kn}}{D_i} \right) & \text{if } \frac{r_{kn}}{D_i} > 0.08 \end{cases} \quad \begin{matrix} \frac{r_{kn}}{D_i} \leq 0.08 = 0 \\ \frac{r_{kn}}{D_i} > 0.08 = 1 \end{matrix} \quad (4.3.15)$$

$$C_{2ts} = 1.2$$

(e) Step 5, internal pressure expected to cause elastic buckling at knuckle

$$P_{eth} := \frac{C_{1ts} \cdot E \cdot t_{ts}^2}{C_{2ts} \cdot R_{th} \cdot (0.5R_{th} - r_{kn})} \quad P_{eth} = 720 \text{ bar} \quad (4.3.16)$$

(f) Step 6, internal pressure expected to result in maximum stress ( $S_y$ ) at knuckle time independent

$$C_{3ts} := S_{y\_304L} \quad S_{y\_304L} := 25000 \text{ psi}$$

$$P_y := \frac{C_{3ts} \cdot t_{ts}}{C_{2ts} \cdot R_{th} \cdot \left( 0.5 \frac{R_{th}}{r_{kn}} - 1 \right)} \quad P_y = 13 \text{ bar} \quad (4.3.17)$$

(g) Step 7 - pressure expected to cause buckling failure of the knuckle

$$\text{for: } G_{th} := \frac{P_{eth}}{P_y} \quad G_{th} = 55.507$$

$$P_{ck} := \left( \frac{0.77508 \cdot G_{th} - 0.20354 \cdot G_{th}^2 + 0.019274 \cdot G_{th}^3}{1 + 0.19014 G_{th} - 0.089534 G_{th}^2 + 0.0093965 G_{th}^3} \right) \cdot P_y \quad P_{ck} = 26 \text{ bar} \quad (4.3.19)$$

(h) Step 8 - allowable pressure based on buckling failure of the knuckle

$$P_{ak} := \frac{P_{ck}}{1.5} \quad P_{ak} = 17.468 \text{ bar}$$

(i) Step 9 - allowable pressure based on rupture of the crown

$$P_{ac} := \frac{2S_{max} \cdot l}{\frac{L_{cr}}{t_{ts}} + 0.5} \quad P_{ac} = 16.6 \text{ bar}$$

(j) Step 10 - maximum allowable internal pressure

$$P = 15.4 \text{ bar}$$

$$P_{a\_ip} := \min(P_{ak}, P_{ac}) \quad P_{a\_ip} = 16.6 \text{ bar}$$

$$P_{a\_ip} > P = 1$$

#### 4.5.10.1 Radial Nozzle in formed head

$$R_n := 5.1\text{cm}$$

$$t_n := 8\text{mm}$$

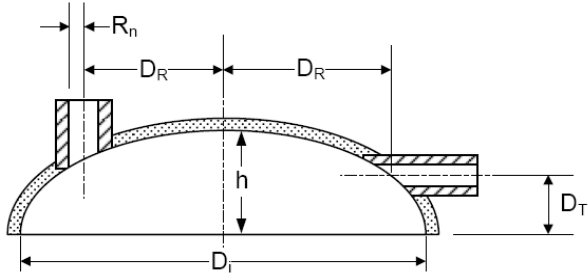
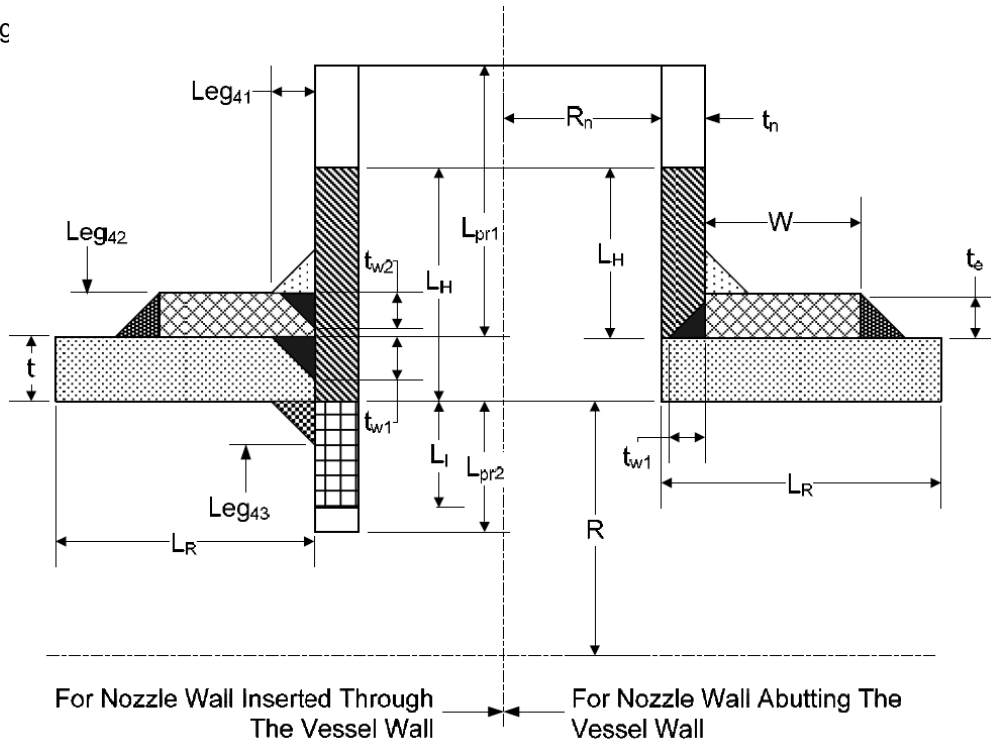


Fig 4.5.11

#### 4.5.10.1 Procedure for Radial Nozzle in a Spherical or Formed head

Fig



a) Step 1

$$R_{\text{eff}} := L_{\text{cr}} \quad R_{\text{eff}} = 1.36 \text{ m} \quad (4.5.64)$$

b) Step 2- limit of reinforcement along vessel wall. Here we compute for both nozzles using parallel calcs

$$D_R := \begin{pmatrix} 0 \\ 10 \end{pmatrix} \text{cm} \quad \text{assume } R_n, t_n \text{ are same for both nozzles}$$

Possible limits of reinforcement:

$$L_{R1} := 0.5 \cdot D_1 - (D_R + R_n + t_n) \quad L_{R1} = \begin{pmatrix} 62.1 \\ 52.1 \end{pmatrix} \text{ cm} \quad (4.5.67)$$

$$\sqrt{R_{\text{eff}} \cdot t_{\text{ts}}} = 11.662 \text{ cm} \quad 2R_n = 10.2 \text{ cm}$$

$$L_{R2} := \min(\sqrt{R_{\text{eff}} \cdot t_{\text{ts}}}, 2R_n) \quad L_{R2} = 10.2 \text{ cm} \quad (4.5.67)$$

Final Limit of reinforcement along vessel wall (assume no pad reinforcement):

$$L_R := \min(L_{R1}, L_{R2}) \quad L_R = 10.2 \text{ cm} \quad (4.5.68)$$

c) Step 3- limit of reinforcement along nozzle wall projecting outside vessel surface wall.

We have no pad reinforcement, and no inside nozzle so:

$$t_e := 0 \text{ mm} \quad L_{\text{pr1}} := 30 \text{ cm} \quad L_{\text{pr2}} := 0 \text{ cm}$$

$$L_H := \min\left[(t_{\text{ts}} + t_e + F_p \cdot \sqrt{R_n \cdot t_n}), L_{\text{pr1}} + t_{\text{ts}}\right] \quad (4.5.73)$$

where:

$$X_o := D_R + R_n + t_n \quad X_o = \begin{pmatrix} 0.059 \\ 0.159 \end{pmatrix} \text{ m} \quad (4.5.79)$$

$$C_p := e^{\frac{0.35D_i - X_o}{8t_{\text{ts}}}} \quad C_p = \begin{pmatrix} 183.552 \\ 52.589 \end{pmatrix} \quad (4.5.78)$$

$$C_n := \min\left[\left(\frac{t_{\text{ts}} + t_e}{t_n}\right)^{0.35}, 1.0\right] \quad C_n = 1 \quad (4.5.81)$$

$$F_p := \min(C_n, C_p) \quad F_p = 1 \quad \text{note that this is true for both values of } C_p, \text{ so we can drop the parallel calculation} \quad (4.5.80)$$

$$L_H := \min\left[(t_{\text{ts}} + t_e + F_p \cdot \sqrt{R_n \cdot t_n}), L_{\text{pr1}} + t_{\text{ts}}\right] \quad L_H = 3.02 \text{ cm} \quad (4.5.73)$$

d) Step 4 - limit of reinforcement along nozzle wall projecting inside vessel surface wall, if applicable

$$L_I := \min(F_p \cdot \sqrt{R_n \cdot t_n}, L_{\text{pr2}}) \quad L_I = 0 \text{ cm} \quad (4.5.82)$$

e) Step 5 - determine total available area near nozzle opening

$$(\text{material strength ratios}) \rightarrow f_{\text{rn}} := 1 \quad f_{\text{rp}} := 1 \quad (4.5.30) \quad (4.5.31)$$

$$A_T := A_1 + f_{\text{rn}}(A_2 + A_3) + A_{41} + A_{42} + A_{43} + f_{\text{rp}} \cdot A_5 \quad (4.5.83)$$

$$A_1 := t_{\text{ts}} \cdot L_R \quad A_1 = 10.2 \text{ cm}^2 \quad (4.5.84)$$

$$A_2 := t_n \cdot L_H \quad A_2 = 2.416 \text{ cm}^2 \quad (4.5.86)$$

$$A_3 := t_n \cdot L_I \quad A_3 = 0 \text{ cm}^2 \quad (4.5.83)$$

$$L_{41} := 0.7 \text{ cm} \quad A_{41} := 0.5 L_{41}^2 \quad A_{41} = 0.245 \text{ cm}^2 \quad (4.5.88)$$

$$L_{42} := 0 \text{ cm} \quad A_{42} := 0.5 L_{42}^2 \quad A_{42} = 0 \text{ cm}^2 \quad (4.5.89)$$

$$L_{43} := 0.7 \text{ cm} \quad A_{43} := 0.5 L_{43}^2 \quad A_{43} = 0.245 \text{ cm}^2 \quad (4.5.90)$$

$$t_e = 0 \text{ cm} \quad A_5 := 0 \text{ cm}^2 \quad (4.5.94)$$

$$A_T := A_1 + f_{rn} \cdot (A_2 + A_3) + A_{41} + A_{42} + A_{43} + f_{rp} \cdot A_5 \quad A_T = 13.106 \text{ cm}^2 \quad (4.5.83)$$

f) Step 6 - determine applicable forces

$$t_{\text{eff}} := t_{ts} \cdot \left( \frac{t_{ts} \cdot L_R + A_5 \cdot f_{rp}}{t_{ts} \cdot L_R} \right) \quad t_{\text{eff}} = 10 \text{ mm} \quad (4.5.100)$$

$$R_{xn} := \frac{t_n}{\ln \left( \frac{R_n + t_n}{R_n} \right)} \quad R_{xn} = 5.49 \text{ cm} \quad R_{xs} := \frac{t_{\text{eff}}}{\ln \left( \frac{R_{\text{eff}} + t_{\text{eff}}}{R_{\text{eff}}} \right)} \quad R_{xs} = 1.365 \text{ m} \quad (4.5.98)$$

$$f_N := P \cdot R_{xn} \cdot (L_H - t_{ts}) \quad f_N = 1.731 \times 10^3 \text{ N} \quad (4.5.95)$$

$$f_S := \frac{P \cdot R_{xs} \cdot (L_R + t_n)}{2} \quad f_S = 1.172 \times 10^5 \text{ N} \quad (4.5.96)$$

$$R_{nc} := R_n \quad (\text{radius along chord} = R_n \text{ for radial nozzles})$$

$$f_T := \frac{P \cdot R_{xs} \cdot R_{nc}}{2} \quad f_T = 5.433 \times 10^4 \text{ N} \quad (4.5.97)$$

g) Step 7 - determine effective thickness for nozzles in spherical, ellipsoidal, or torispherical heads

$$t_{\text{eff}} = 1 \text{ cm} \quad \text{same formula as above in step 6} \quad (4.5.100)$$

h) Step 8 - Determine avg. local primary membrane stress and general primary membrane stress at nozzle intersection

$$\sigma_{\text{avg}} := \frac{f_N + f_S + f_T}{A_T} \quad \sigma_{\text{avg}} = 132.2 \text{ MPa} \quad (4.5.101)$$

$$\sigma_{\text{circ}} := \frac{P \cdot R_{xs}}{2 t_{\text{eff}}} \quad \sigma_{\text{circ}} = 106.5 \text{ MPa} \quad (4.5.102)$$

i) Step 9 Determine maximum local primary membrane stress

$$P_L := \max \left[ (2 \sigma_{\text{avg}} - \sigma_{\text{circ}}), \sigma_{\text{circ}} \right] \quad P_L = 157.8 \text{ MPa} \quad (4.5.103)$$

$$E_w = 1$$

$$S_{\text{allow}} := 1.5 S_{\text{max}} \cdot E_w \quad S_{\text{allow}} = 172.7 \text{ MPa} \quad (4.5.43)$$

j) Step 10 - Maximum local primary membrane stress must be less than the allowable stress

$$P_L \leq S_{\text{allow}} = 1 \quad (4.5.104)$$

k) Step 11 - Determine max allowable working pressure of the nozzle